

# Development of 10 kW-scale hydrogen generator using chemical hydride

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## Abstract

We have developed a hydrogen generator that generates high purity hydrogen gas from the aqueous solution of sodium borohydride, NaBH<sub>4</sub>. This paper discussed the performance testing of the hydrogen generator using a Pt-LiCoO<sub>2</sub>-coated honeycomb monolith. The NaBH<sub>4</sub> solution hydrolyzed to generate H<sub>2</sub> and sodium metaborate when it contacted the monolith. The gravimetric and the volumetric H<sub>2</sub> densities of the system were 2 wt.% and 1.5 kg H<sub>2</sub>/100l, respectively. The volumetric density was similar to that of the compressed H<sub>2</sub> at 25 MPa. The hydrogen generator successfully provided a maximum H<sub>2</sub> generation rate of 120 nl/min. Assuming a standard PEM (polymer electrolyte fuel cell, PEFC) fuel cell operated at 0.7 V, generating 120 nl/min was equivalent to 12 kW.

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**Keywords:** Sodium borohydride; Chemical hydride; Hydrogen generator; Catalyst; Hydrogen; Fuel cell

## 1. Introduction

A fuel cell is a battery, which is actuated with hydrogen (H<sub>2</sub>) and oxygen (O<sub>2</sub>). The energy obtained by a reaction of H<sub>2</sub> and O<sub>2</sub> is directly converted into electric energy. Since such a fuel cell has efficiency much higher than that of conventional combustion engines, a fuel cell vehicle (FCV) is expected as a car having high efficiency [1,2]. A polymer electrolyte fuel cell (PEFC) is the prime power source for a FCV, as well as another application called a fuel cell uninterrupted power supply (FCUPS). One of the most widely envisioned sources of fuel for FCV or FCUPS is H<sub>2</sub>. Therefore, it is necessary to have a storage tank of H<sub>2</sub> to start the system on demand.

H<sub>2</sub> can be stored in tanks of compressed [2,3] or liquefied H<sub>2</sub> [3], or by adsorption on activated carbon [4], carbon nanotubes [3,5,6] and graphite nanofiber [7,8] or in a hydrogen-absorbing alloy [9] or in a chemical hydride such as NaBH<sub>4</sub> [10–18], NaH [19], LiH [20], or NaAlH<sub>4</sub> [21]. Among these methods, attention has been given to the hydrolysis of a chemical hydride such as NaBH<sub>4</sub> [10–18] because of the large theoretical H<sub>2</sub> content of 10.9 wt.%. NaBH<sub>4</sub> is stable compared with other chemical hydrides and is easy to handle. At room temperatures, only a small

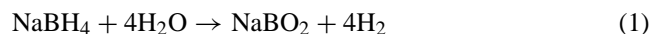
percentage of the theoretical amount of H<sub>2</sub> was liberated by hydrolysis reaction of NaBH<sub>4</sub> and H<sub>2</sub>O [14,22], but the hydrolysis is enhanced by using catalysts. Conventionally known catalysts are metal halides, colloidal platinum, activated carbon, Raney nickel [10], fluorinated Mg-based hydride [16] or ruthenium supported on anion exchange resin [17,18], as well as cobalt and nickel borides [11,13].

In a previous paper, metal-metal oxide such as Pt-LiCoO<sub>2</sub> was found to work as an excellent catalyst for releasing H<sub>2</sub> by hydrolysis of NaBH<sub>4</sub> solution [22]. The catalyst produced 100% of the theoretical amount of H<sub>2</sub> using excess water (H<sub>2</sub>O/NaBH<sub>4</sub> = 210 mol/mol). Furthermore, it was demonstrated that NaBO<sub>2</sub> was recycled back to NaBH<sub>4</sub> using coke or methane [23]. In this paper, we have constructed a 10 kW-scale hydrogen generator using NaBH<sub>4</sub> as the hydrogen storage material and Pt-LiCoO<sub>2</sub> as the catalyst for releasing H<sub>2</sub>. The system produced a maximum H<sub>2</sub> generation rate of 120 nl/min.

## 2. Experimental

### 2.1. Materials

Sodium borohydride (Rohm and Haas, NaBH<sub>4</sub>) was used for the reaction with water. The reaction of NaBH<sub>4</sub> and H<sub>2</sub>O is shown as follows [10]:



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The  $\text{NaBH}_4$  solution hydrolyzes to yield  $\text{H}_2$  gas and sodium metaborate ( $\text{NaBO}_2$ ). In our system,  $\text{Pt-LiCoO}_2$  catalyst was selected based on our previous results [22]. We investigated various metal catalysts coated on a metal oxide and found that  $\text{Pt-LiCoO}_2$  worked as an excellent catalyst for releasing  $\text{H}_2$  from the  $\text{NaBH}_4$  solution. The  $\text{Pt-LiCoO}_2$  catalyst was synthesized using a conventional impregnation method as described in the previous paper [22]. Dinitrodiammine platinum(II) nitric acid solution ( $\text{Pt}(\text{NO}_2)_2(\text{NH}_3)_2$ , 33 ml, Pt content of 50 g/l, Tanaka Kikinzoku Kogyo K.K., Japan) and lithium cobaltate powder ( $\text{LiCoO}_2$ , Nippon Chemical Industries Co. Ltd., product name Cellseed 5) were mixed. The mixture was held at 523 K for 5 h. The dried powder was calcined for 2 h in air at 723 K, thereby coating Pt on the metal oxide. Thus, the  $\text{Pt-LiCoO}_2$  catalyst contained a Pt content of 1.5 wt.%.

The hydride reactor of our hydrogen generator contains a honeycomb monolith of 150 mm in length and 130 mm in diameter coated with  $\text{Pt-LiCoO}_2$  (monolith: 808 g;  $\text{Pt-LiCoO}_2$ : 240 g;  $\text{Al}_2\text{O}_3$ : 60 g). The  $\text{Pt-LiCoO}_2$ -coated monolith was prepared by the following method.  $\text{Pt-LiCoO}_2$  (1000 g),  $\text{Al}_2\text{O}_3$  sol (620 g,  $\text{Al}_2\text{O}_3$  20 wt.%) and water (125 g) were mixed with an attritor. A cordierite monolith was dipped into the slurry. After removing the slurry, the monolith was dried at 393 K for 24 h. The dried monolith was calcined for 3 h in air at 723 K. The features of the monolith are  $\text{Pt-LiCoO}_2$  loading of 0.30 g per 1 g substrate, 400 cells per square inch with 21% blockage resulting in a single channel diameter of approximately 1.2 mm.

## 2.2. Hydrogen generator

A general schematic diagram for our hydrogen generator is shown in Fig. 1. The hydrogen generator is made up of a fuel tank for a  $\text{NaBH}_4$  solution, a pump for the solution, the byproduct ( $\text{NaBO}_2$ ) solution storage tank, a separator (internal volume 4 l) and a hydride reactor (internal volume 2 l). The material of the fuel tank, the byproduct tank, the separator, the reactor and the piping material were SUS 304 stainless steel. The reactor contained a honeycomb monolith coated with  $\text{Pt-LiCoO}_2$  catalyst. Fig. 2 shows the overview photograph of our generator. The size of the body is 380 mm  $\times$  650 mm  $\times$  800 mm.

The amounts of  $\text{H}_2$  generated using the generator were determined as follows. For the hydrogen generator,  $\text{NaBH}_4$

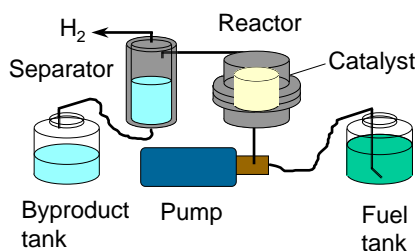


Fig. 1. Schematic diagram of hydrogen generator.



Fig. 2. Overview photograph of hydrogen generator.

solution (3.8–25 wt.%) entered the bottom of the reactor contained the honeycomb monolith via a pump at 296 K and flowed upward through the channel. The solution flow rate was controlled from 25 to 300 ml/min using the pump. By contacting the honeycomb monolith, the fuel solution generated  $\text{H}_2$  gas and  $\text{NaBO}_2$  (in solution) with a temperature rise. The outlet temperature was measured directly behind the monolith exit of the reactor using a thermocouple. The  $\text{H}_2$  gas and the  $\text{NaBO}_2$  solution were separated by the separator, which also acted as a small storage buffer for  $\text{H}_2$  gas. The  $\text{H}_2$  generation rate was detected by a Micro Motion flow meter (CMF010) consist of Corioli's sensor and a microprocessor-based transmitter which installed behind the separator.

## 2.3. Characterization

Crystalline structure of the byproduct by the hydrolysis reaction of  $\text{NaBH}_4$  was investigated by wide angle X-ray diffraction. The X-ray diffraction pattern was recorded at room temperature by using a Rigaku Denki Rad-B over a range of diffraction angle ( $2\theta$ ) from 3 to  $80^\circ$  with Cu K $\alpha$  radiation (30 kV, 30 mA) filtered by a monochromator.

## 3. Results and discussion

The  $\text{H}_2$  generation rate as a function of time for 3.8 wt.%  $\text{NaBH}_4$  solution and constant feed of 300 ml/min is shown in Fig. 3. When we start feeding the  $\text{NaBH}_4$  solution into the  $\text{Pt-LiCoO}_2$ -coated honeycomb monolith of the generator

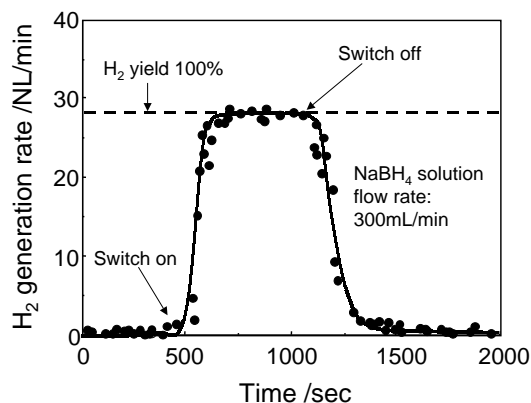


Fig. 3. Response of hydrogen generator.

by switching on the pump, the H<sub>2</sub> gas starts to generate. After 200 s, the H<sub>2</sub> generation rate reaches a constant value of 27 nl/min. By switching off the pump, the H<sub>2</sub> generation ceases in 200 s. The response is stable and independent of the concentration and the feed rate.

The H<sub>2</sub> generation rate ( $V_h$ , nl/min) at the H<sub>2</sub> yield of 100% was determined by the following equation:

$$V_h = (0.213W_s V_s d) \times 11.2 = 2.39W_s V_s d \quad (2)$$

where  $W_s$  (wt.%) is the concentration of NaBH<sub>4</sub>,  $V_s$  (ml/min) is the NaBH<sub>4</sub> solution flow rate, and  $d$  (g/cm<sup>3</sup>) is the density of the NaBH<sub>4</sub> solution. The densities of NaBH<sub>4</sub>, water and NaOH are 1.07 [24], 1.00 [24] and 2.13 g/cm<sup>3</sup> [24], respectively. We calculated the density of the NaBH<sub>4</sub> solution by addition relationship of their densities. The values of 0.213 and 11.2 are the theoretical amount of H<sub>2</sub> generated per unit weight of NaBH<sub>4</sub> and the volume (nl) occupied by the 1 g of H<sub>2</sub> at STP (273 K, 1 atm), respectively. The dotted line in Fig. 3 is the H<sub>2</sub> generation rate at the H<sub>2</sub> yield of 100%. We found that all NaBH<sub>4</sub> is consumed by heterogeneous reactions on the catalytic Pt-LiCoO<sub>2</sub> coating. Without the catalyst in the generator, the H<sub>2</sub> generation rate was 0–1 nl/min. The NaBH<sub>4</sub> solution is quite stable when maintained at a

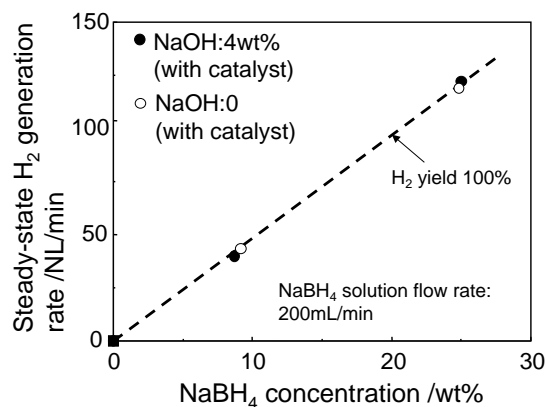
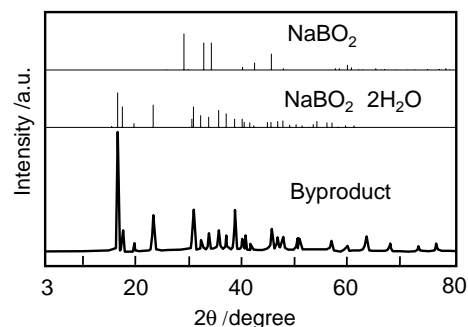
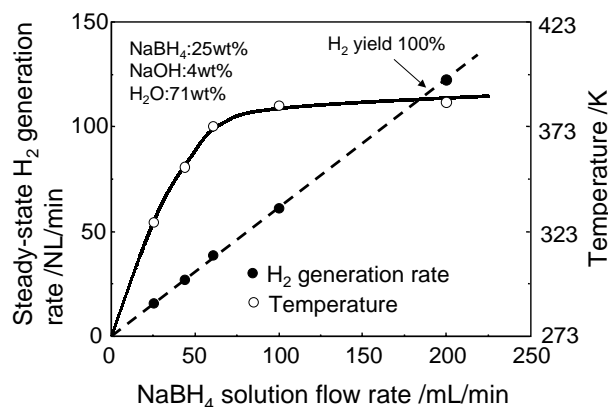
Fig. 4. Influence of NaBH<sub>4</sub> solution concentration on steady-state H<sub>2</sub> generation rate.

Fig. 5. X-ray diffraction intensity curve of byproduct.

high pH [17,18]. In our experiment, H<sub>2</sub> did not generate above and including 4 wt.% NaOH (pH 14) at temperatures below 323 K.

The H<sub>2</sub> generation rate was measured in 4 wt.% NaOH and 8.6–25 wt.% NaBH<sub>4</sub> water solution. The steady-state H<sub>2</sub> generation rates as a function of the NaBH<sub>4</sub> concentration are shown in Fig. 4. As the NaBH<sub>4</sub> concentration is increased, the H<sub>2</sub> generation rate linearly increases and reaches a value of 120 nl/min at 25 wt.%. Amendola et al. reported that as weight percent NaOH increased, H<sub>2</sub> generation rate decreased [18]. But, the H<sub>2</sub> generation rate using our generator is independent of the NaOH concentration as shown in Fig. 4. This may be due to the fact that the Pt-LiCoO<sub>2</sub> catalyst has high activity. It is also noted in Fig. 4 that 100% of the stoichiometric amount of H<sub>2</sub> was generated by the reactor as long as the concentration is below 25 wt.% and the H<sub>2</sub> generation rate is below 120 nl/min. X-ray diffraction was used to estimate the structure of the byproduct obtained from the solution (NaBH<sub>4</sub> concentration: 25 wt.%). Fig. 5 illustrates the X-ray diffraction intensity curve of the byproduct together with those of NaBO<sub>2</sub> [25] and NaBO<sub>2</sub>·2H<sub>2</sub>O [26]. The diffraction peaks of the byproduct are from NaBO<sub>2</sub>·2H<sub>2</sub>O, as shown in the figure.

Fig. 6 shows the effect of the NaBH<sub>4</sub> solution flow rate on the steady-state H<sub>2</sub> generation rate and the outlet temperature at the 25 wt.% NaBH<sub>4</sub> and 4 wt.% NaOH solution.

Fig. 6. Influence of NaBH<sub>4</sub> solution flow rate on steady-state H<sub>2</sub> generation rate.

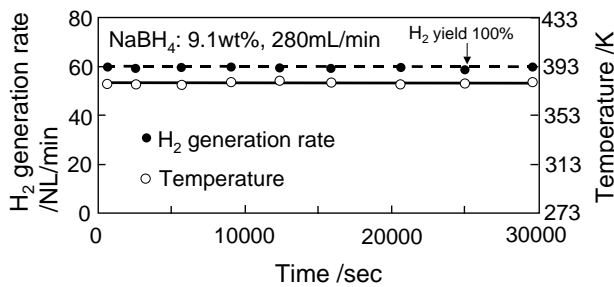


Fig. 7. Durability of hydrogen generator.

As the  $\text{NaBH}_4$  flow rate increases, the  $\text{H}_2$  generation rate increases and reaches 120 nl/min at the rate of 200 ml/min. The temperature of the byproduct solution increased rapidly inside the reactor due to the high exothermic reaction [22]. This temperature was measured directly behind the monolith. After the  $\text{NaBH}_4$  solution was fed, the temperature increased and had a constant value when the flow rate was constant. The temperature increases with the  $\text{NaBH}_4$  flow rate and shows a value of 384 K at 200 ml/min.

Temperature dependencies of the solubility of  $\text{NaBH}_4$  and  $\text{NaBO}_2$  were determined by visual observation. In our experiment, the solubility of  $\text{NaBO}_2$  and  $\text{NaBH}_4$  is shown as follows:

$$\text{solubility of NaBH}_4 \text{ (g/100 g water)} = -261 + 1.05T \quad (3)$$

$$\text{solubility of NaBO}_2 \text{ (g/100 g water)} = -245 + 0.915T \quad (4)$$

where  $T$  is the temperature (K).

Eqs. (3) and (4) indicate that the solubility of  $\text{NaBO}_2$  decreases compared with that of  $\text{NaBH}_4$  and the concentration of  $\text{NaBH}_4$  should be below 26 wt.% at 333 K in order to keep the byproduct ( $\text{NaBO}_2$ ) a solution state.

Durability is one of the major criteria for the generator. Fig. 7 shows the outlet temperature of the byproduct solution and the steady-state  $\text{H}_2$  generation rate as a function of time. The generator shows during 30,000 s no decrease of the  $\text{H}_2$  generation rate. At the steady-state, the temperature of the byproduct solution is 373 K for the following conditions:  $\text{NaBH}_4$  solution feed 280 ml/min,  $\text{NaBH}_4$  concentration 9.1 wt.%.

Table 1 shows the specification of our hydrogen generator. The gravimetric and the volumetric  $\text{H}_2$  densities of the generator containing the fuel tank and the byproduct tank are 1.3 wt.% and 0.5 kg/100l, respectively. Assuming that the ratio of weight/volume of the tanks is constant (12 kg/25 l), those densities increase with the size of the fuel tank and the byproduct tank (gravimetric  $\text{H}_2$  density: 2 wt.%; volumetric  $\text{H}_2$  density: 1.5 kg  $\text{H}_2$ /100l; fuel tank: 60 kg, 125 l; byproduct: 60 kg, 125 l). The volumetric  $\text{H}_2$  density is similar to that of a compressed  $\text{H}_2$  system at 25 MPa, because to store 1.3 kg of  $\text{H}_2$  requires a volume of 100l at 25 MPa.

Table 1  
Specification of hydrogen generator

Hydrogen (nl/min)	120
Fuel flow (nl/min)	200
Body size	380 mm × 650 mm × 800 mm 197.61
Weight (kg)	80
Tank size	Fuel tank (25 l, 12 kg) Byproduct tank (25 l, 12 kg)
Gravimetric hydrogen density (wt.%)	1.3–2.0
Volumetric hydrogen density (kg/100l)	0.5–1.5
Fuel content: $\text{NaBH}_4$ (wt.%)	25
Catalyst: Pt-LiCoO <sub>2</sub> (g)	240

The volumetric  $\text{H}_2$  density was calculated by assuming that a ratio of outer/inner volume is 1.2 [3,27].

We can estimate power levels using our system. Assuming a standard PEM (PEFC) fuel cell operating at 0.7 V, generating 120 nl/min (0.18 g  $\text{H}_2$ /s) is equivalent to 12 kW (0.18 mol/s × 96,500 C/mol × 0.7 V = 17 kA × 0.7 V). Our hydrogen generator is used to power a specially designed 10 kW  $\text{H}_2$ /air PEM fuel cell. The fuel cell consumes  $\text{NaBH}_4$  and generates  $\text{NaBO}_2$  solution. The high gravimetric and volumetric  $\text{H}_2$  densities in our chemical hydride system without using high  $\text{H}_2$  pressure may be highly effective as a  $\text{H}_2$  storage system for FCV, FCUPS or for any emergency power source.

#### 4. Conclusions

We have developed a 10 kW-scale hydrogen generator that generates high purity  $\text{H}_2$  gas from aqueous solutions of  $\text{NaBH}_4$ . The generator was made up of a fuel tank for the  $\text{NaBH}_4$  solution, a pump for the solution, the byproduct ( $\text{NaBO}_2$ ) solution storage tank, a separator and a hydride reactor. The reactor contained a honeycomb monolith coated with Pt-LiCoO<sub>2</sub> catalyst. The maximum  $\text{H}_2$  generation rate was 120 nl/min. The gravimetric and the volumetric  $\text{H}_2$  densities of the system were 2 wt.% and 1.5 kg/100l, respectively.

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